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SYMMETRICALLY ACTUATED INK EJECTION COMPONENTS FOR AN INK JET PRINTHEAD CHIP

FIELD OF THE INVENTION

This invention relates to a printhead chip for an ink jet printhead. More particularly, this invention relates to a printhead chip that includes a plurality of symmetrically actuated, moving nozzle arrangements.

BACKGROUND OF THE INVENTION

10 As set out in the above referenced applications/patents, the Applicant has spent a substantial amount of time and effort in developing printheads that incorporate micro electro-mechanical system (MEMS) – based components to achieve the ejection of ink necessary for printing.

As a result of the Applicant's research and development, the Applicant has been able to develop printheads having one or more printhead chips that together incorporate up to 84 000 nozzle arrangements. The Applicant has also developed suitable processor technology that is capable of controlling operation of such printheads. In particular, the processor technology and the printheads are capable of cooperating to generate resolutions of 1600 dpi and higher in some cases. Examples of suitable processor technology are
20 provided in the above referenced patent applications/patents.

The Applicant has overcome substantial difficulties in achieving the necessary ink flow and ink drop separation within the ink jet printheads.

As can be noted in the above referenced patents/patent applications, a number of printhead chips developed by the Applicant include a structure that defines an ink ejection port. The structure is displaceable with respect to the substrate to eject ink from a nozzle chamber. This is a result of the displacement of the structure reducing a volume of ink within the nozzle chamber. A particular difficulty with such a configuration is achieving a sufficient extent and speed of movement of the structure to achieve ink drop ejection. On the microscopic scale of the nozzle arrangements, this extent and speed of movement can
30 be achieved to a large degree by ensuring that movement of the ink ejection structure is as efficient as possible.

The Applicant has conceived this invention to achieve such efficiency of movement.

SUMMARY OF THE INVENTION

According to the invention, there is provided a printhead chip for an ink jet printhead, the printhead chip comprising

a substrate; and

a plurality of nozzle arrangements that are positioned on the substrate, each nozzle arrangement comprising

an active ink ejection structure that is positioned on the substrate and spaced from the substrate, the active ink ejection structure having a roof with an ink ejection port defined in the roof;

a static ink ejection structure positioned on the substrate, the active ink ejection structure and the static ink ejection structure together defining a nozzle chamber in fluid communication with an ink supply, the active ink ejection structure being displaceable with respect to the static ink ejection structure towards and away from the substrate to reduce and increase a volume of the nozzle chamber to eject an ink drop from the nozzle chamber; and

at least two actuators that are operatively arranged with respect to the active ink ejection structure to displace the active ink ejection structure with respect to the static ink ejection structure towards and away from the substrate, the actuators being configured and connected to the active ink ejection structure to impart substantially rectilinear movement to the active ink ejection structure.

The invention is now described, by way of example, with reference to the accompanying drawings. The following description is not intended to limit the broad scope of the above summary.

BRIEF DESCRIPTION OF THE DRAWINGS

In the drawings,

Figure 1 shows a three-dimensional view of a nozzle arrangement of a first embodiment of a printhead chip in accordance with the invention, for an ink jet printhead;

Figure 2 shows a three-dimensional sectioned view of the nozzle arrangement of Figure 1;

Figure 3 shows a transverse cross sectional view of a thermal bend actuator of the nozzle arrangement of Figure 1;

Figure 4 shows a three-dimensional sectioned view of the nozzle arrangement of Figure 1, in an initial stage of ink drop ejection;

Figure 5 shows a three-dimensional sectioned view of the nozzle arrangement of Figure 1, in a terminal stage of ink drop ejection;

Figure 6 shows a schematic view of one coupling structure of the nozzle arrangement of Figure 1;

Figure 7 shows a schematic view of a part of the coupling structure attached to an active ink ejection structure of the nozzle arrangement, when the nozzle arrangement is in a quiescent condition;

10 Figure 8 shows the part of Figure 7 when the nozzle arrangement is in an operative condition;

Figure 9 shows an intermediate section of a connecting plate of the coupling structure, when the nozzle arrangement is in a quiescent condition;

Figure 10 shows the intermediate section of Figure 9, when the nozzle arrangement is in an operative condition;

Figure 11 shows a schematic view of a part of the coupling structure attached to a connecting member of the nozzle arrangement when the nozzle arrangement is in a quiescent condition;

20 Figure 12 shows the part of Figure 11 when the nozzle arrangement is in an operative condition; and

Figure 13 shows a plan view of a nozzle arrangement of a second embodiment of a printhead chip, in accordance with the invention, for an ink jet printhead.

DETAILED DESCRIPTION OF THE INVENTION

In Figures 1 to 5, reference numeral 10 generally indicates a nozzle arrangement of a printhead chip, in accordance with the invention, for an ink jet printhead.

30 The nozzle arrangement 10 is one of a plurality of such nozzle arrangements formed on a silicon wafer substrate 12 to define the printhead chip of the invention. As set out in the background of this specification, a single printhead can contain up to 84 000 such nozzle arrangements. For the purposes of clarity and ease of description, only one nozzle arrangement is described. It is to be appreciated that a person of ordinary skill in the field can readily obtain the printhead chip by simply replicating the nozzle arrangement 10 on the wafer substrate 12.

The printhead chip is the product of an integrated circuit fabrication technique. In particular, each nozzle arrangement 10 is the product of a MEMS – based fabrication technique. As is known, such a fabrication technique involves the deposition of functional layers and sacrificial layers of integrated circuit materials. The functional layers are etched to define various moving components and the sacrificial layers are etched away to release the components. As is known, such fabrication techniques generally involve the replication of a large number of similar components on a single wafer that is subsequently diced to separate the various components from each other. This reinforces the submission that a person of ordinary skill in the field can readily obtain the printhead chip of this invention by replicating the nozzle arrangement 10.

An electrical drive circuitry layer 14 is positioned on the silicon wafer substrate 12. The electrical drive circuitry layer 14 includes CMOS drive circuitry. The particular configuration of the CMOS drive circuitry is not important to this description and has therefore not been shown in any detail in the drawings. Suffice to say that it is connected to a suitable microprocessor and provides electrical current to the nozzle arrangement 10 upon receipt of an enabling signal from said suitable microprocessor. An example of a suitable microprocessor is described in the above referenced patents/patent applications. It follows that this level of detail will not be set out in this specification.

An ink passivation layer 16 is positioned on the drive circuitry layer 14. The ink passivation layer 16 can be of any suitable material, such as silicon nitride.

The nozzle arrangement 10 includes an ink inlet channel 18 that is one of a plurality of such ink inlet channels defined in the substrate 12.

The nozzle arrangement 10 includes an active ink ejection structure 20. The active ink ejection structure 20 has a roof 22 and sidewalls 24 that depend from the roof 22. An ink ejection port 26 is defined in the roof 22.

The active ink ejection structure 20 is connected to, and between, a pair of thermal bend actuators 28 with coupling structures 30 that are described in further detail below. The roof 22 is generally rectangular in plan and, more particularly, can be square in plan. This is simply to facilitate connection of the actuators 28 to the roof 22 and is not critical. For example, in the event that three actuators are provided, the roof 22 could be generally triangular in plan. There may thus be other shapes that are suitable.

The active ink ejection structure 20 is connected between the thermal bend actuators 28 so that a free edge 32 of the sidewalls 24 is spaced from the ink passivation layer 16. It

will be appreciated that the sidewalls 24 bound a region between the roof 22 and the substrate 12.

The roof 22 is generally planar, but defines a nozzle rim 76 that bounds the ink ejection port 26. The roof 22 also defines a recess 78 positioned about the nozzle rim 76 which serves to inhibit ink spread in case of ink wetting beyond the nozzle rim 76.

The nozzle arrangement 10 includes a static ink ejection structure 34 that extends from the substrate 12 towards the roof 22 and into the region bounded by the sidewalls 24. The static ink ejection structure 34 and the active ink ejection structure 20 together define a nozzle chamber 42 in fluid communication with an opening 38 of the ink inlet channel 18.

10 The static ink ejection structure 34 has a wall portion 36 that bounds an opening 38 of the ink inlet channel 18. An ink displacement formation 40 is positioned on the wall portion 36 and defines an ink displacement area that is sufficiently large so as to facilitate ejection of ink from the ink ejection port 26 when the active ink displacement structure 20 is displaced towards the substrate 12. The opening 38 is substantially aligned with the ink ejection port 26.

The thermal bend actuators 28 are substantially identical. It follows that, provided a similar driving signal is supplied to each thermal bend actuator 28, the thermal bend actuators 28 each produce substantially the same force on the active ink ejection structure 20.

20 In Figure 3 there is shown the thermal bend actuator 28 in further detail. The thermal bend actuator 28 includes an arm 44 that has a unitary structure. The arm 44 is of an electrically conductive material that has a coefficient of thermal expansion which is such that a suitable component of such material is capable of performing work, on a MEMS scale, upon expansion and contraction of the component when heated and subsequently cooled. The material can be one of many. However, it is desirable that the material has a Young's Modulus that is such that, when the component bends through differential heating, energy stored in the component is released when the component cools to assist return of the component to a starting condition. The Applicant has found that a suitable material is Titanium Aluminum Nitride (TiAlN). However, other conductive materials may also be
30 suitable, depending on their respective coefficients of thermal expansion and Young's Modulus.

The arm 44 has a pair of outer passive portions 46 and a pair of inner active portions 48. The outer passive portions 46 have passive anchors 50 that are each made fast with the

ink passivation layer 16 by a retaining structure 52 of successive layers of titanium and silicon dioxide or equivalent material.

The inner active portions 48 have active anchors 54 that are each made fast with the drive circuitry layer 14 and are electrically connected to the drive circuitry layer 14. This is also achieved with a retaining structure 56 of successive layers of titanium and silicon dioxide or equivalent material.

10 The arm 44 has a working end that is defined by a bridge portion 58 that interconnects the portions 46, 48. It follows that, with the active anchors 54 connected to suitable electrical contacts in the drive circuitry layer 14, the inner active portions 48 define an electrical circuit. Further, the portions 46, 48 have a suitable electrical resistance so that the inner active portions 48 are heated when a current from the CMOS drive circuitry passes through the inner active portions 48. It will be appreciated that substantially no current will pass through the outer passive portions 46 resulting in the passive portions heating to a significantly lesser extent than the inner active portions 48. Thus, the inner active portions 48 expand to a greater extent than the outer passive portions 46.

20 As can be seen in Figure 3, each outer passive portion 46 has a pair of outer horizontally extending sections 60 and a central horizontally extending section 62. The central section 62 is connected to the outer sections 60 with a pair of vertically extending sections 64 so that the central section 62 is positioned intermediate the substrate 12 and the outer sections 60.

Each inner active portion 48 has a transverse profile that is effectively an inverse of the outer passive portions 46. Thus, outer sections 66 of the inner active portions 48 are generally coplanar with the outer sections 60 of the passive portions 46 and are positioned intermediate central sections 68 of the inner active portions 48 and the substrate 12. It follows that the inner active portions 48 define a volume that is positioned further from the substrate 12 than the outer passive portions 46. It will therefore be appreciated that the greater expansion of the inner active portions 48 results in the arm 44 bending towards the substrate 12. This movement of the arms 44 is transferred to the active ink ejection structure 20 to displace the active ink ejection structure 20 towards the substrate 12.

30 This bending of the arms 44 and subsequent displacement of the active ink ejection structure 20 towards the substrate 12 is indicated in Figure 4. The current supplied by the CMOS drive circuitry is such that an extent and speed of movement of the active ink displacement structure 20 causes the formation of an ink drop 70 outside of the ink ejection

port 26. When the current in the inner active portions 48 is discontinued, the inner active portions 48 cool, causing the arm 44 to return to a position shown in Figure 1. As discussed above, the material of the arm 44 is such that a release of energy built up in the passive portions 46 assists the return of the arm 44 to its starting condition. In particular, the arm 44 is configured so that the arm 44 returns to its starting position with sufficient speed to cause separation of the ink drop 70 from ink 72 within the nozzle chamber 42.

On the macroscopic scale, it would be counter-intuitive to use heat expansion and contraction of material to achieve movement of a functional component. However, the Applicant has found that, on a microscopic scale, the movement resulting from heat expansion is fast enough to permit a functional component to perform work. This is particularly so when suitable materials, such as TiAlN are selected for the functional component.

One coupling structure 30 is mounted on each bridge portion 58. As set out above, the coupling structures 30 are positioned between respective thermal actuators 28 and the roof 22. It will be appreciated that the bridge portion 58 of each thermal actuator 28 traces an arcuate path when the arm 44 is bent and straightened in the manner described above. Thus, the bridge portions 58 of the oppositely oriented actuators 28 tend to move away from each other when actuated, while the active ink ejection structure 20 maintains a rectilinear path. It follows that the coupling structures 30 should accommodate movement in two axes, in order to function effectively.

Details of one of the coupling structures 30 are shown in Figures 6. It will be appreciated that the other coupling structure 30 is simply an inverse of that shown in Figure 6. It follows that it is convenient to describe just one of the coupling structures 30.

The coupling structure 30 includes a connecting member 74 that is positioned on the bridge portion 58 of the thermal actuator 28. The connecting member 74 has a generally planar surface 80 that is substantially coplanar with the roof 22 when the nozzle arrangement 10 is in a quiescent condition.

A pair of spaced proximal tongues 82 is positioned on the connecting member 74 to extend towards the roof 22. Likewise, a pair of spaced distal tongues 84 is positioned on the roof 22 to extend towards the connecting member 74 so that the tongues 82, 84 overlap in a common plane parallel to the substrate 12. The tongues 82 are interposed between the tongues 84.

A rod 86 extends from each of the tongues 82 towards the substrate 12. Likewise, a rod 88 extends from each of the tongues 84 towards the substrate 12. The rods 86, 88 are substantially identical. The connecting structure 30 includes a connecting plate 90. The plate 90 is interposed between the tongues 82, 84 and the substrate 12. The plate 90 interconnects ends 92 of the rods 86, 88. Thus, the tongues 82, 84 are connected to each other with the rods 86, 88 and the connecting plate 90.

During fabrication of the nozzle arrangement 10, layers of material that are deposited and subsequently etched include layers of TiAlN, titanium and silicon dioxide. Thus, the thermal actuators 28, the connecting plates 90 and the static ink ejection structure 34 are of TiAlN. Further, both the retaining structures 52, 56, and the connecting members 74 are composite, having a layer 94 of titanium and a layer 96 of silicon dioxide positioned on the layer 74. The layer 74 is shaped to nest with the bridge portion 58 of the thermal actuator 28. The rods 86, 88 and the sidewalls 24 are of titanium. The tongues 82, 84 and the roof 22 are of silicon dioxide.

When the CMOS drive circuitry sets up a suitable current in the thermal bend actuator 28, the connecting member 74 is driven in an arcuate path as indicated with an arrow 98 in Figure 6. This results in a thrust being exerted on the connecting plate 90 by the rods 86. One actuator 28 is positioned on each of a pair of opposed sides 100 of the roof 22 as described above. It follows that the downward thrust is transmitted to the roof 22 such that the roof 22 and the distal tongues 84 move on a rectilinear path towards the substrate 12. The thrust is transmitted to the roof 22 with the rods 88 and the tongues 84.

The rods 86, 88 and the connecting plate 90 are dimensioned so that the rods 86, 88 and the connecting plate 90 can distort to accommodate relative displacement of the roof 22 and the connecting member 74 when the roof 22 is displaced towards the substrate 12 during the ejection of ink from the ink ejection port 26. The titanium of the rods 86, 88 has a Young's Modulus that is sufficient to allow the rods 86, 88 to return to a straightened condition when the roof 22 is displaced away from the ink ejection port 26. The TiAlN of the connecting plate 90 also has a Young's Modulus that is sufficient to allow the connecting plate 90 to return to a starting condition when the roof 22 is displaced away from the ink ejection port 26. The manner in which the rods 86, 88 and the connecting plate 90 are distorted is indicated in Figures 7 to 12.

For the sake of convenience, the substrate 12 is assumed to be horizontal so that ink drop ejection is in a vertical direction.

As can be seen in Figures 11 and 12, when the thermal bend actuator 28 receives a current from the CMOS drive circuitry, the connecting member 74 is driven towards the substrate 12 as set out above. This serves to displace the connecting plate 90 towards the substrate 12. In turn, the connecting plate 90 draws the roof 22 towards the substrate 12 with the rods 88. As described above, the displacement of the roof 22 is rectilinear and therefore vertical. It follows that displacement of the distal tongues 84 is constrained on a vertical path. However, displacement of the proximal tongues 82 is arcuate and has both vertical and horizontal components, the horizontal components being generally away from the roof 22. The distortion of the rods 86, 88 and the connecting plate 90 therefore
10 accommodates the horizontal component of movement of the proximal tongues 82.

In particular, the rods 86 bend and the connecting plate 90 rotates partially as shown in Figure 12. In this operative condition, the proximal tongues 82 are angled with respect to the substrate. This serves to accommodate the position of the proximal tongues 82. As set out above, the distal tongues 84 remain in a rectilinear path as indicated by an arrow 102 in Figure 8. Thus, the rods 88 that bend as shown in Figure 8 as a result of a torque transmitted by the plate 90 resist the partial rotation of the connecting plate 90. It will be appreciated that an intermediate part 104 between each rod 86 and its adjacent rod 88 is also subjected to a partial rotation, although not to the same extent as the part shown in Figure 12. The part shown in Figure 8 is subjected to the least amount of rotation due to the
20 fact that resistance to such rotation is greatest at the rods 88. It follows that the connecting plate 90 is partially twisted along its length to accommodate the different extents of rotation. This partial twisting allows the plate 90 to act as a torsional spring thereby facilitating separation of the ink drop 70 when the roof 22 is displaced away from the substrate 12.

At this point, it is to be understood that the tongues 82, 84, the rods 86, 88 and the connecting plate 90 are all fast with each other so that relative movement of these components is not achieved by any relative sliding movement between these components.

It follows that bending of the rods 86, 88 sets up three bend nodes in each of the rods 86, 88, since pivotal movement of the rods 86, 88 relative to the tongues 82, 84 is
30 inhibited. This enhances an operative resilience of the rods 86, 88 and therefore also facilitates separation of the ink drop 70 when the roof 22 is displaced away from the substrate 12.

In Figure 13, reference numeral 110 generally indicates a nozzle arrangement of a second embodiment of a printhead chip, in accordance with the invention, for an ink jet printhead. With reference to Figures 1 to 12, like reference numerals refer to like parts, unless otherwise specified.

The nozzle arrangement 110 includes four symmetrically arranged thermal bend actuators 28. Each thermal bend actuator 28 is connected to a respective side 112 of the roof 22. The thermal bend actuators 28 are substantially identical to ensure that the roof 22 is displaced in a rectilinear manner.

10 The static ink ejection structure 34 has an inner wall 116 and an outer wall 118 that together define the wall portion 36. An inwardly directed ledge 114 is positioned on the inner wall 116 and extends into the nozzle chamber 42.

A sealing formation 120 is positioned on the outer wall 118 to extend outwardly from the wall portion 38. It follows that the sealing formation 120 and the ledge 114 define the ink displacement formation 40.

The sealing formation 120 includes a re-entrant portion 122 that opens towards the substrate 12. A lip 124 is positioned on the re-entrant portion 122 to extend horizontally from the re-entrant portion 122. The sealing formation 120 and the sidewalls 24 are configured so that, when the nozzle arrangement 10 is in a quiescent condition, the lip 124 and a free edge 126 of the sidewalls 24 are in horizontal alignment with each other. A
20 distance between the lip 124 and the free edge 126 is such that a meniscus is defined between the sealing formation 120 and the free edge 126 when the nozzle chamber 42 is filled with the ink 72. When the nozzle arrangement 10 is in an operative condition, the free edge 126 is interposed between the lip 124 and the substrate 12 and the meniscus stretches to accommodate this movement. It follows that when the chamber 42 is filled with the ink 72, a fluidic seal is defined between the sealing formation 120 and the free edge 126 of the sidewalls 24.

The Applicant believes that the invention provides a means whereby substantially rectilinear movement of an ink-ejecting component can be achieved. The Applicant has found that this form of movement enhances efficiency of operation of the nozzle
30 arrangement 10. Further, the rectilinear movement of the active ink ejection structure 20 results in clean drop formation and separation, a characteristic that is the primary goal of ink jet printhead manufacturers.